

# Performance evaluation of ethanol production through continuous fermentation

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# Talk Outline

- Background
- The Model
- Results
- Possible impact of work – Economic analysis
- Conclusions and Future work

# Background

- Kyoto Protocol and recent surge in oil prices has renewed interest in biofuels
- Largest ethanol fuel industries exists in Brazil (based on sugarcane) and USA (based on corn).
- In Brazil: 50% of all cars are able to use 100% ethanol fuels and gasoline sold contains at least 20% ethanol.
- The energy content of ethanol is approximately two-thirds that of petrol by volume.
- It takes only six months to harvest a substantial crop for fuel.

# The Model — biochemistry

A.B. Jarzebski. (1992). “Modelling of oscillatory behaviour in continuous ethanol fermentation”. *Biotechnology Letters*, **14**(2), 137–142.

- Substrate ( $S$ ) - glucose.
- Product - ethanol - ( $P$ )
- Biomass (*Zymomonos mobilis*)
  - Viable cells ( $X_v$ )
  - Non-viable cells ( $X_{nv}$ ) — non-growing, but still retain the ability to produce ethanol.
  - Dead cells ( $X_d$ ) — eqn uncouples.

Jarzebski (1992) estimated parameter values using experimental data from Perego *et al* (1985).

# Model — single reactor

$$V \frac{dS}{dt} = F(S_0 - S) - V \left( \frac{\mu_v X_v}{Y_{x|s}} + m_s X_{nv} \right),$$

$$V \frac{dX_v}{dt} = -F X_v + V(\mu_v - \mu_{nv} - \mu_d) X_v,$$

$$V \frac{dX_{nv}}{dt} = -F X_{nv} + V(\mu_{nv} X_v - \mu_d X_{nv}),$$

$$V \frac{dX_d}{dt} = -K_d + V \mu_d (X_v + X_{nv}),$$

$$V \frac{dP}{dt} = -F P + V \left( \frac{\mu_v X_v}{Y_{x|p}} + m_p X_{nv} \right).$$

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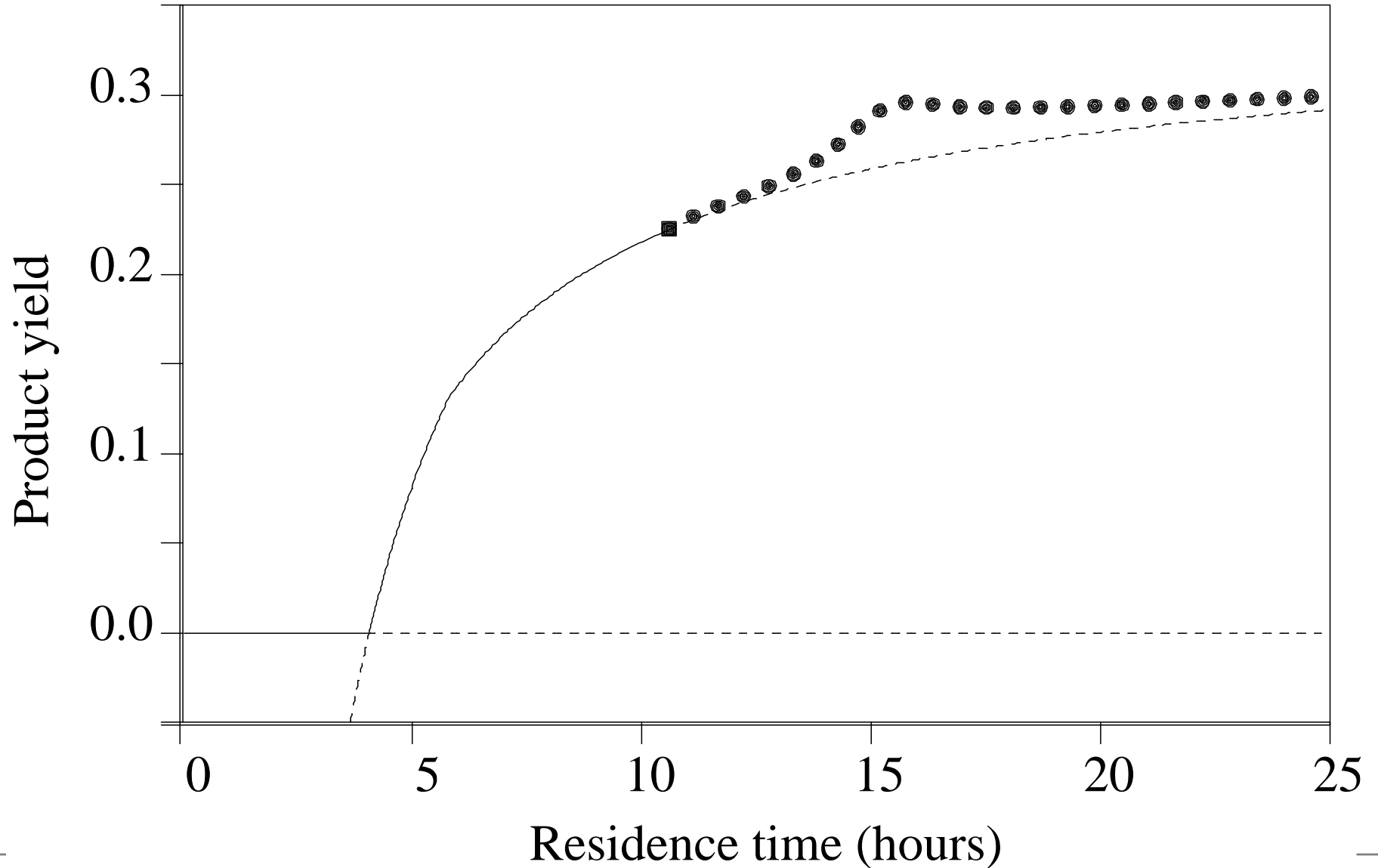
# Performance (1)

We characterise the performance of the reactor system by its product yield at the outlet:

$$\text{Ethanol yield} = \frac{P_i - P_0}{S^0}$$

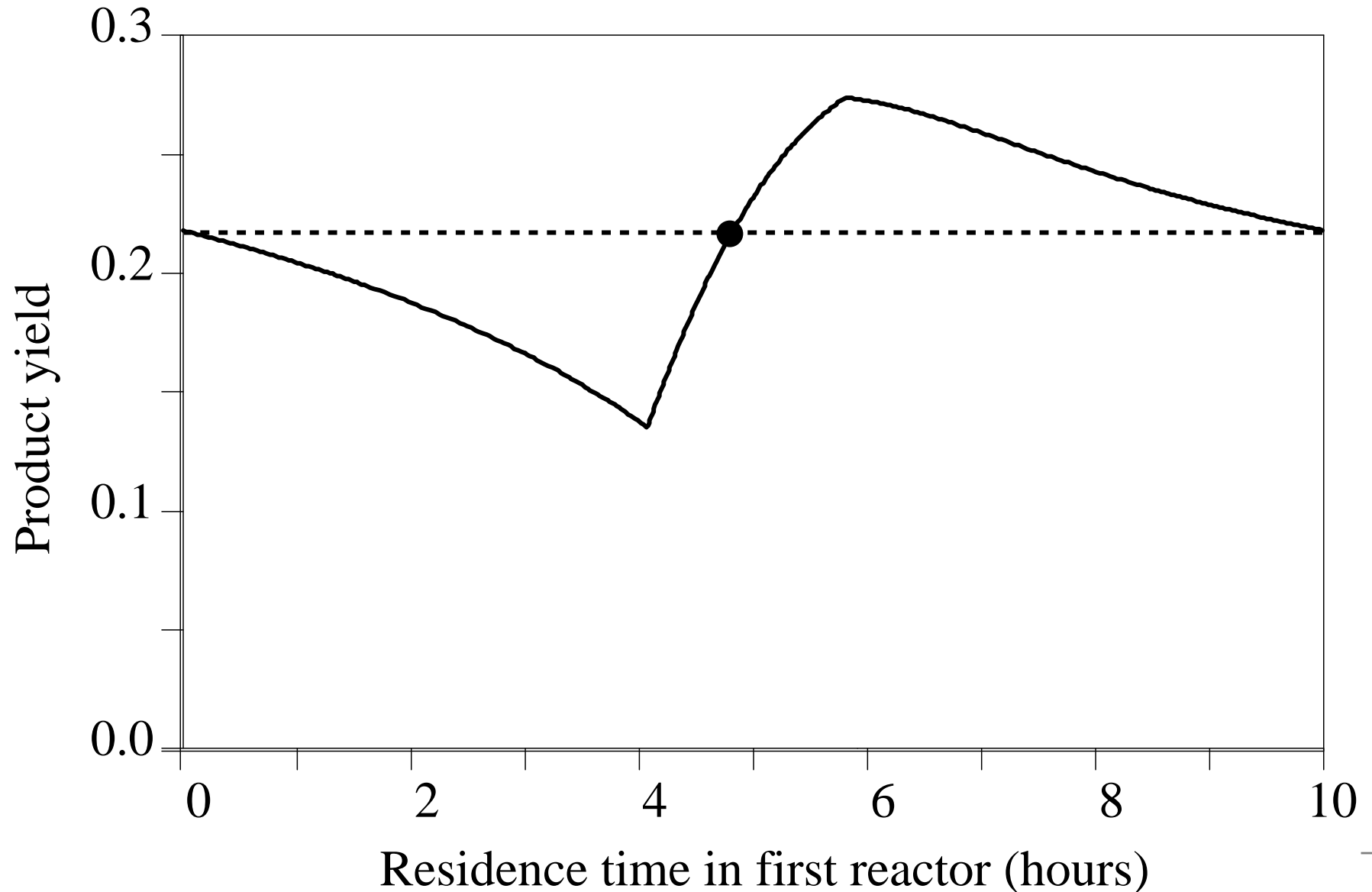
We assume that the concentration of ethanol at the influent of the fermenter is zero, ie.  $P_0 = 0$ .

# Performance: single fermenter



# Performance: a two-reactor cascade (1)

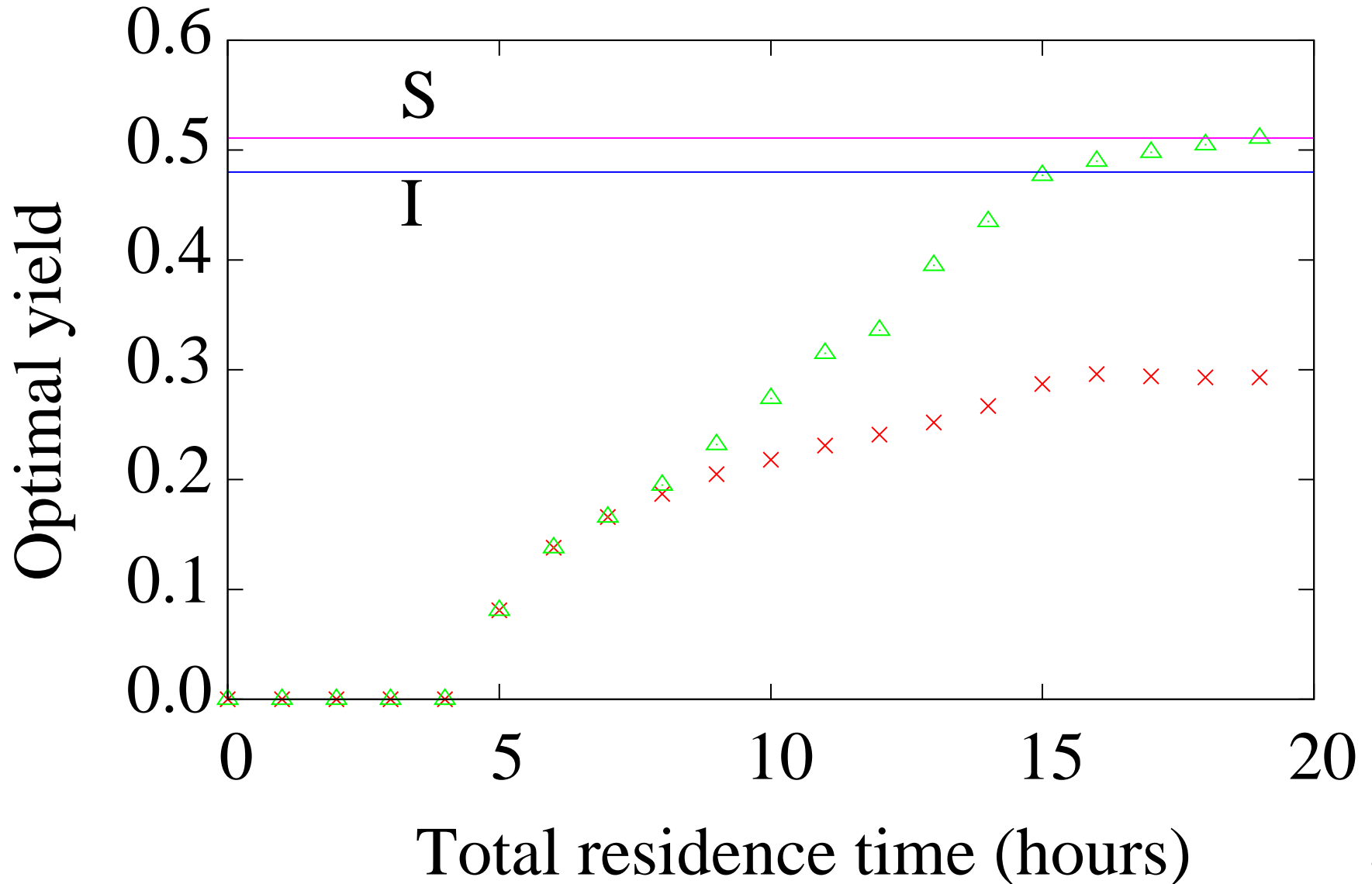
( $\tau_{cr} = 4.83$ )



# Performance: a two-reactor cascade (2)

$Y(\tau_{total} = 15.23) = 0.48$

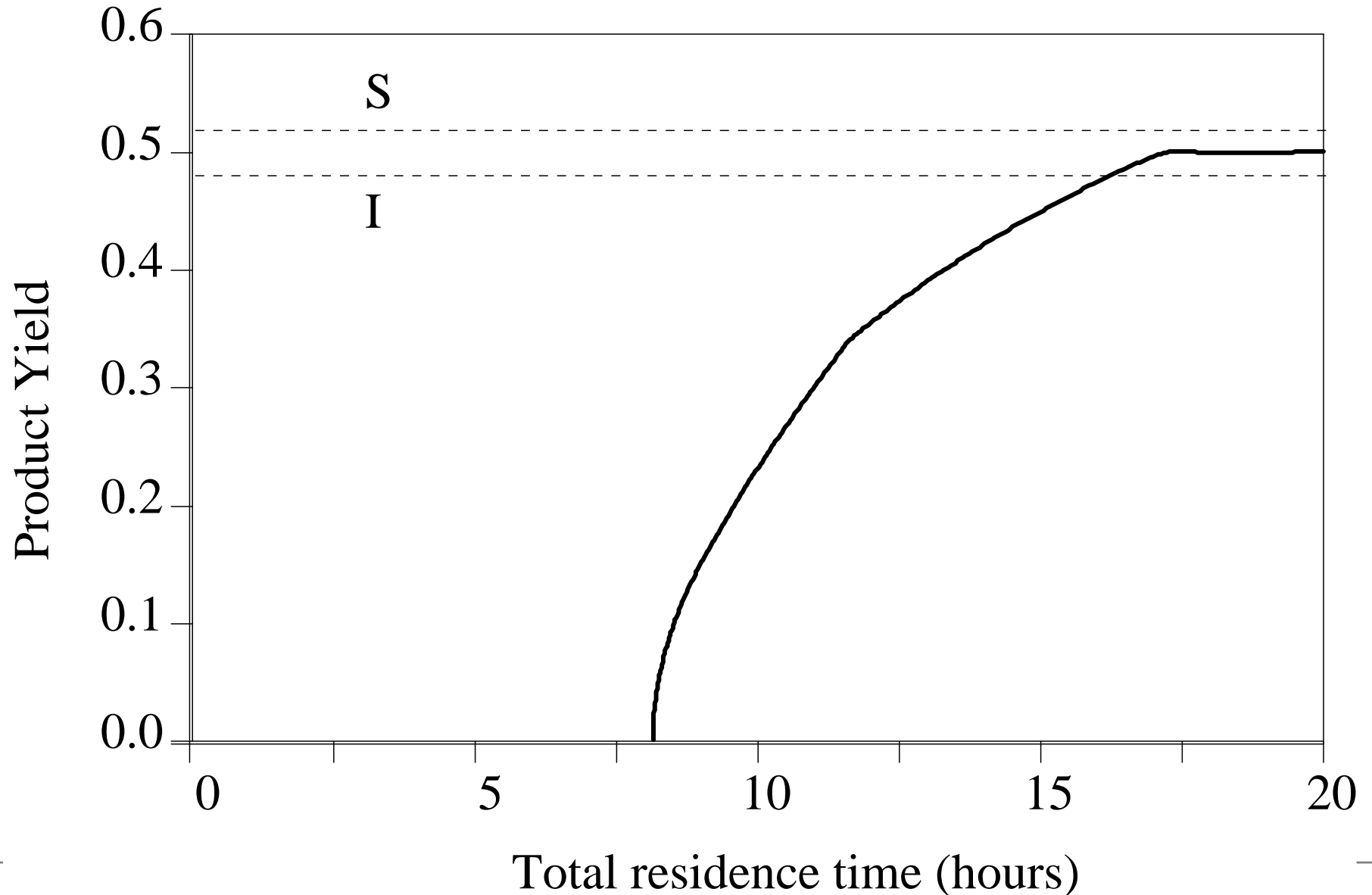
Approaches stoichiometric values for  $\tau_{total} = 19$  hours



# Double reactor cascade ( $\tau_i = \tau_t/2$ )

$Y(\tau_{total} = 16.22) = 0.48$

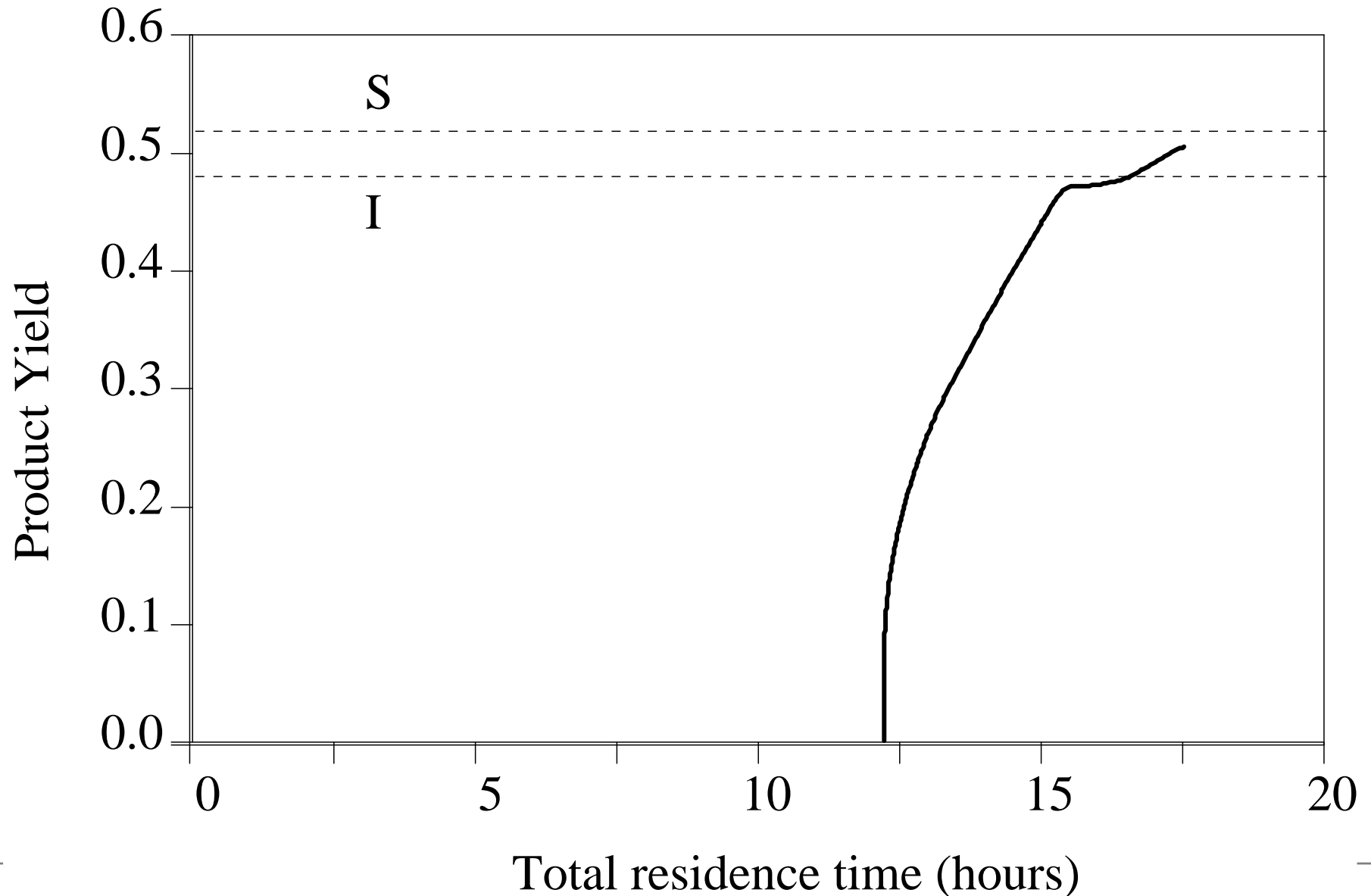
Approaches stoichiometric values for  $\tau_{total} = 20$  hours



# Triple reactor cascade ( $\tau_i = \tau_t/3$ )

$Y(\tau_{total} = 16.29) = 0.48$

Approaches stoichiometric values for  $\tau_{total} = 17.55$  hours



Back of envelope calculations” @

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- Assuming current corn price of \$4.00/bu (US) and ethanol of \$4.00/gal (US) and a current yield of 0.48 gal ethanol/bu (US), increasing the yield to an industrial standard (0.48) to 0.51 gal ethanol/bu (US) would result in \$3.36/bu (US) additional income for a typical 25 million bu (US) corn crop.

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- Assuming current corn price of \$4.00/gal (US) and ethanol of \$4.00/gal (US), increasing the yield of ethanol from the industrial standard (0.48) to 0.51 would result in \$3.36 million additional income for a typical 25 million gallon ethanol plant.
- Approximately 97% of this value is due to increased ethanol production/decreased feedstocks, with the remaining 3% due to reduced energy requirements.

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- For sufficiently large total residence times, the cascade can outperform the single reactor.
- Determined reactor designs which can give product yield higher than 0.48.
- Simulations were able to achieve product yields close to the stoichiometric values.
- Main contribution is not the specific reactor designs that were found to give yields over 0.48 but the systematic approach of using path following methods.

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- Investigate different substrate concentration in the feeds and the inclusion of recycle.

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- The use of a permselective membrane module and a cell/substrate separator to separate the cell and unused substrate from the exit stream to be recycled back into the first tank.